

# Numerical Precision in the LAPW Method

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# APW+lo: energy derivative of order 1

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$$\phi_{\mathbf{k}+\mathbf{G}}(\mathbf{S}_\alpha + \mathbf{r}) = \sum_{lm} A_{lm}^\alpha(\mathbf{k} + \mathbf{G}) u_l^\alpha(r, E_l) Y_{lm}(\hat{\mathbf{r}})$$

$$\phi_{lo}^{lm}(\mathbf{S}_\alpha + \mathbf{r}) = [\tilde{A}_{lm}^\alpha u_l^\alpha(r, E_l) + \tilde{C}_{lm}^\alpha \dot{u}_l^\alpha(r, E_l)] Y_{lm}(\hat{\mathbf{r}})$$

"APW+1lo"

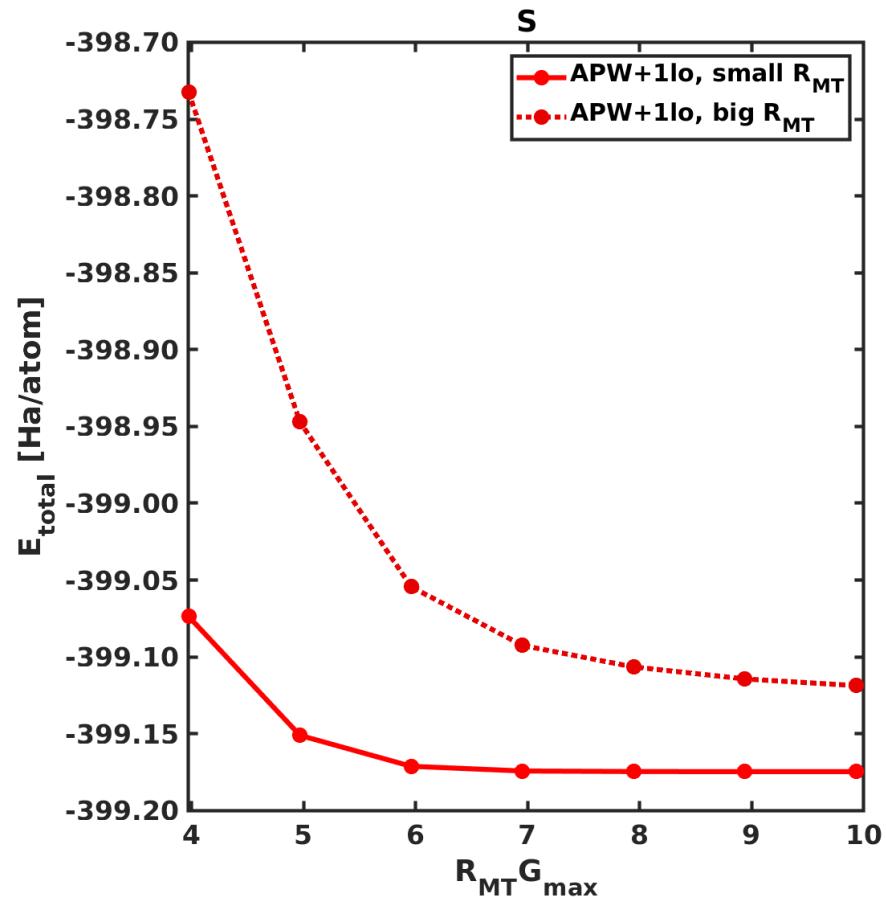
Check quality of basis by changing muffin-tin radius

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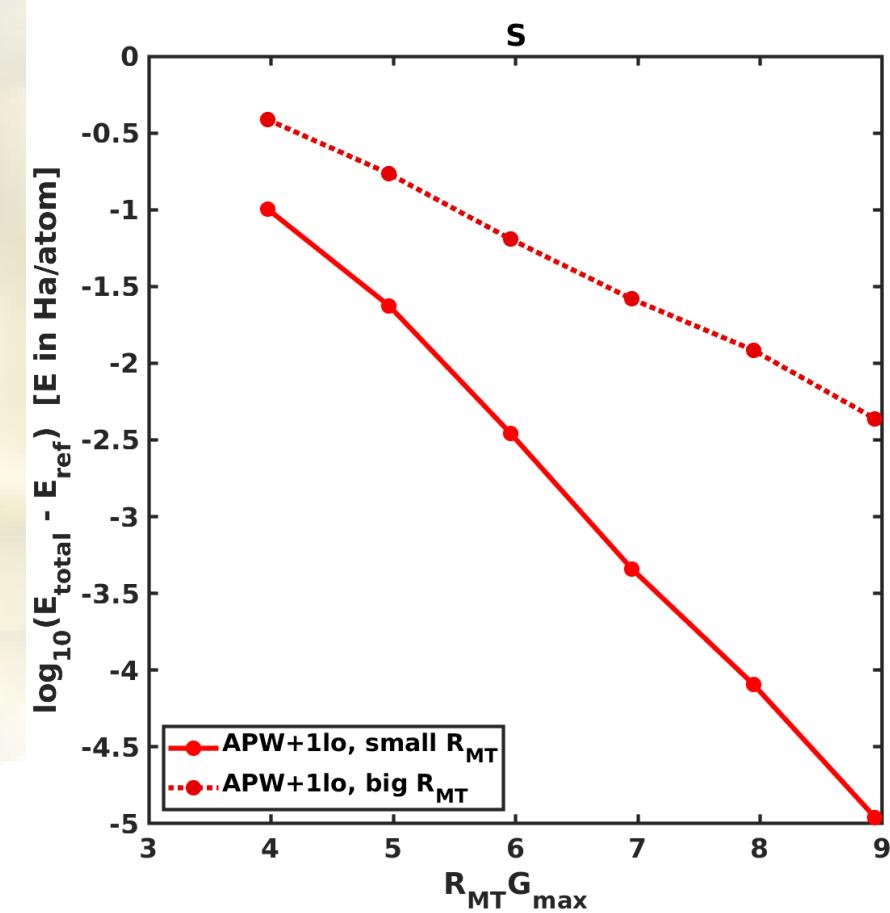
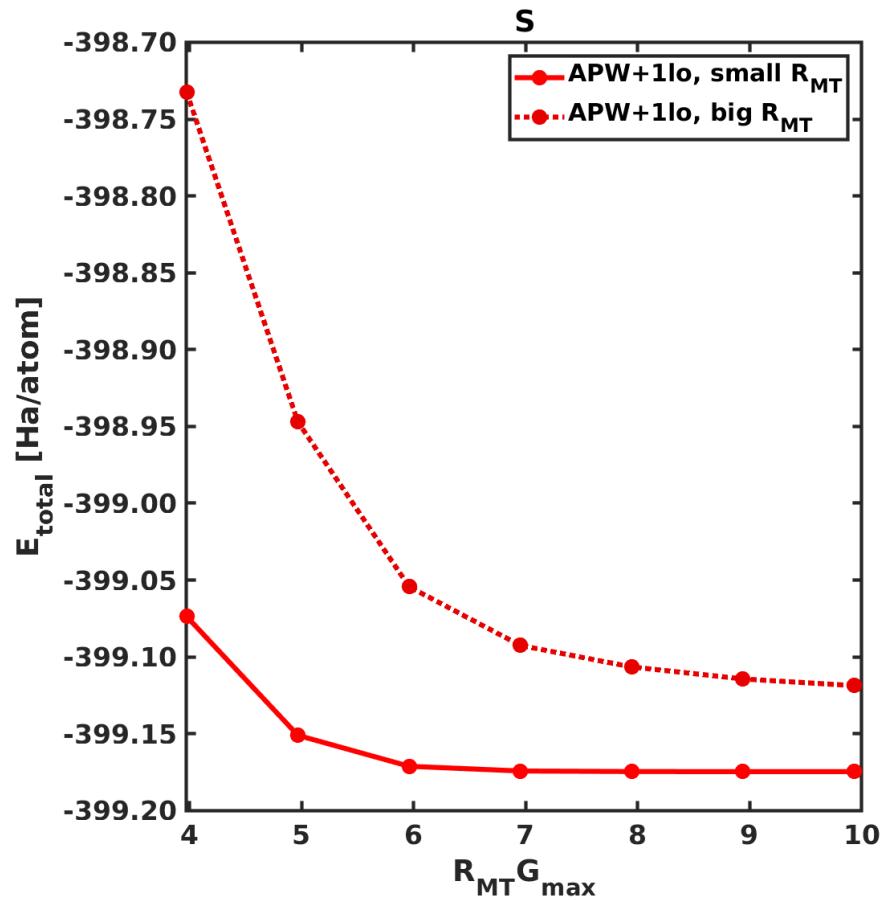
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# APW+lo: influence of muffin-tin radii



(R<sub>MT</sub> G<sub>max</sub> ≡ rgkmax)

# APW+lo: influence of muffin-tin radii



# APW+lo: energy derivative of order 1 & 2

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$$\phi_{\mathbf{k}+\mathbf{G}}(\mathbf{S}_\alpha + \mathbf{r}) = \sum_{lm} A_{lm}^\alpha(\mathbf{k} + \mathbf{G}) u_l^\alpha(r, E_l) Y_{lm}(\hat{\mathbf{r}})$$

&

$$\phi_{lo}^{lm}(\mathbf{S}_\alpha + \mathbf{r}) = [\tilde{A}_{lm}^\alpha u_l^\alpha(r, E_l) + \tilde{C}_{lm}^\alpha \dot{u}_l^\alpha(r, E_l)] Y_{lm}(\hat{\mathbf{r}})$$

$$\phi_{lo}^{lm}(\mathbf{S}_\alpha + \mathbf{r}) = [\tilde{\tilde{A}}_{lm}^\alpha u_l^\alpha(r, E_l) + \tilde{\tilde{C}}_{lm}^\alpha \ddot{u}_l^\alpha(r, E_l)] Y_{lm}(\hat{\mathbf{r}})$$

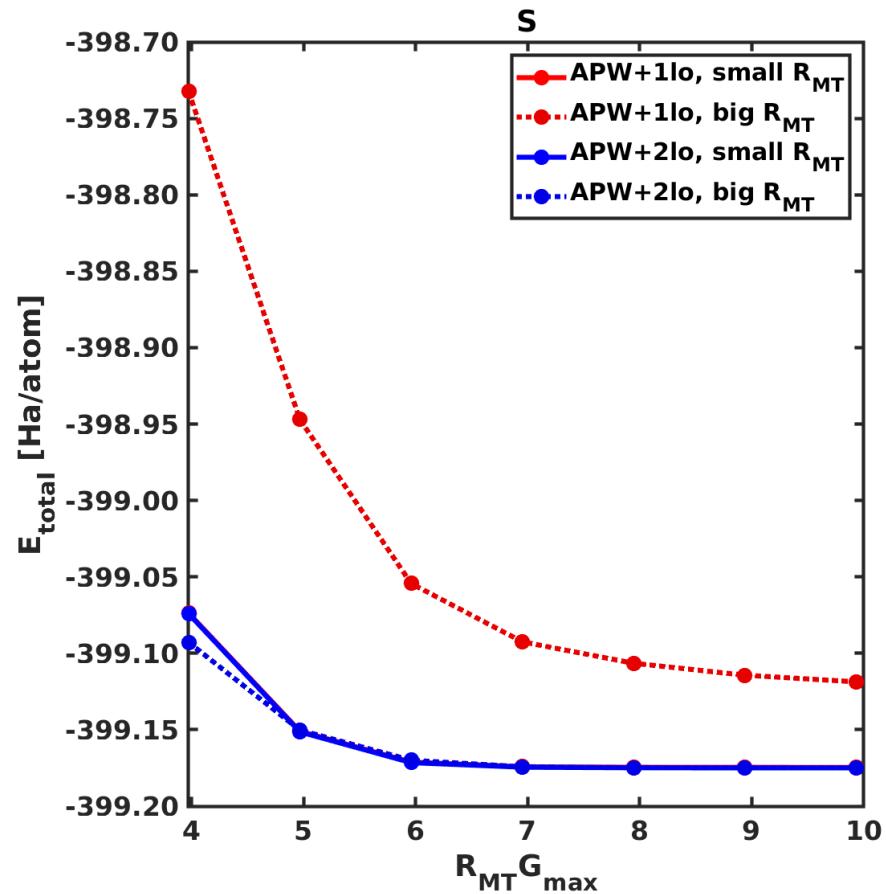
} "APW+2lo"

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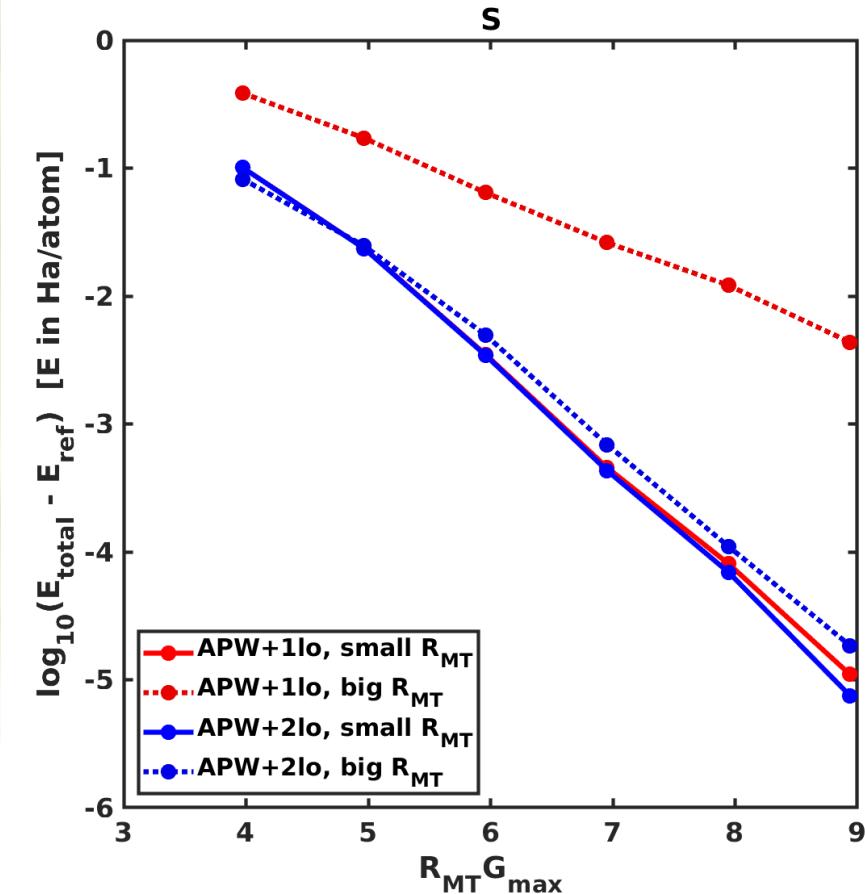
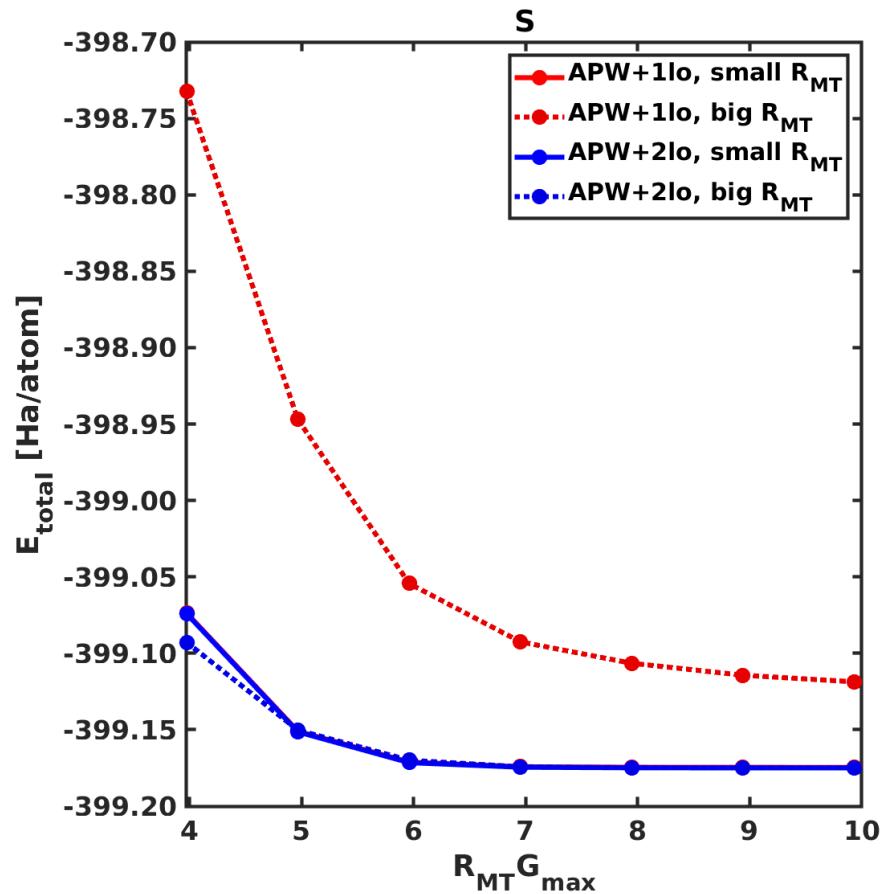


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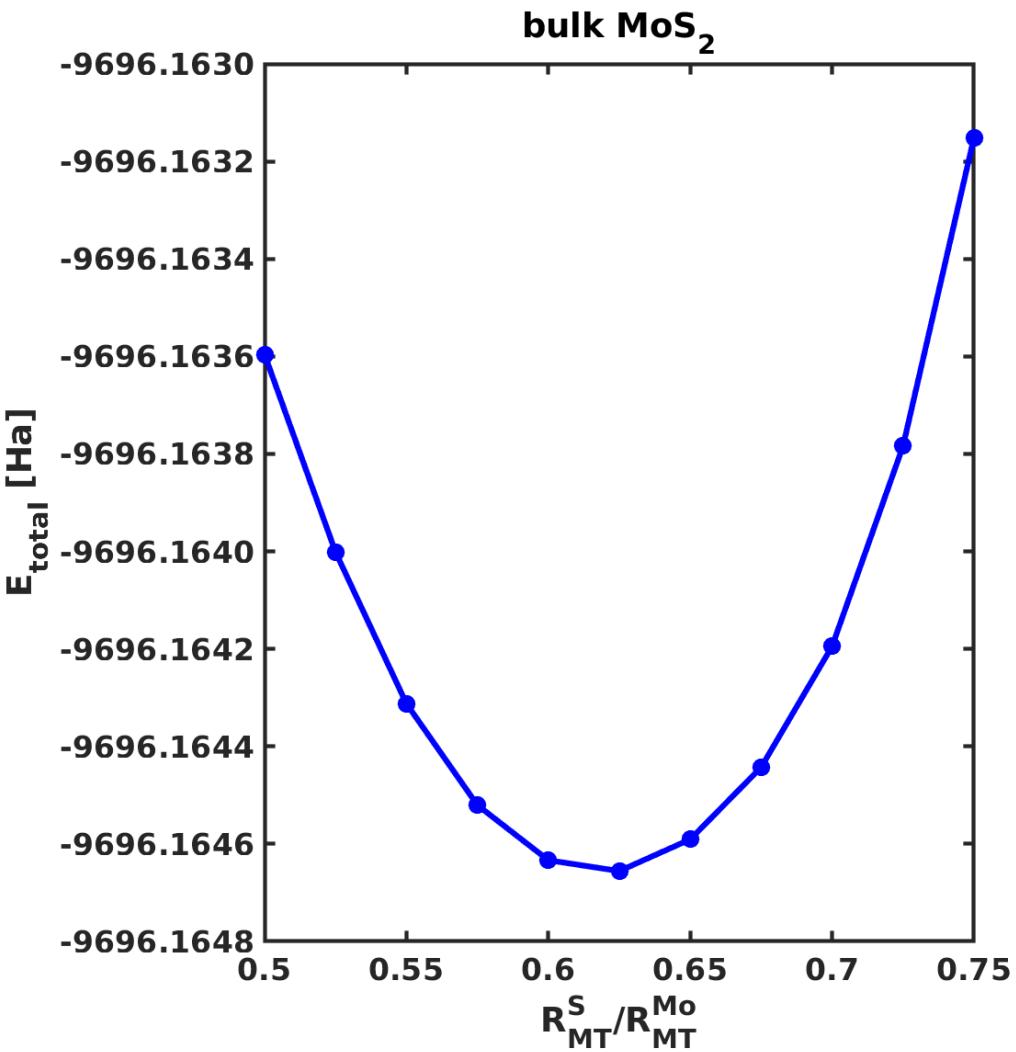
# APW+lo: influence of muffin-tin radii



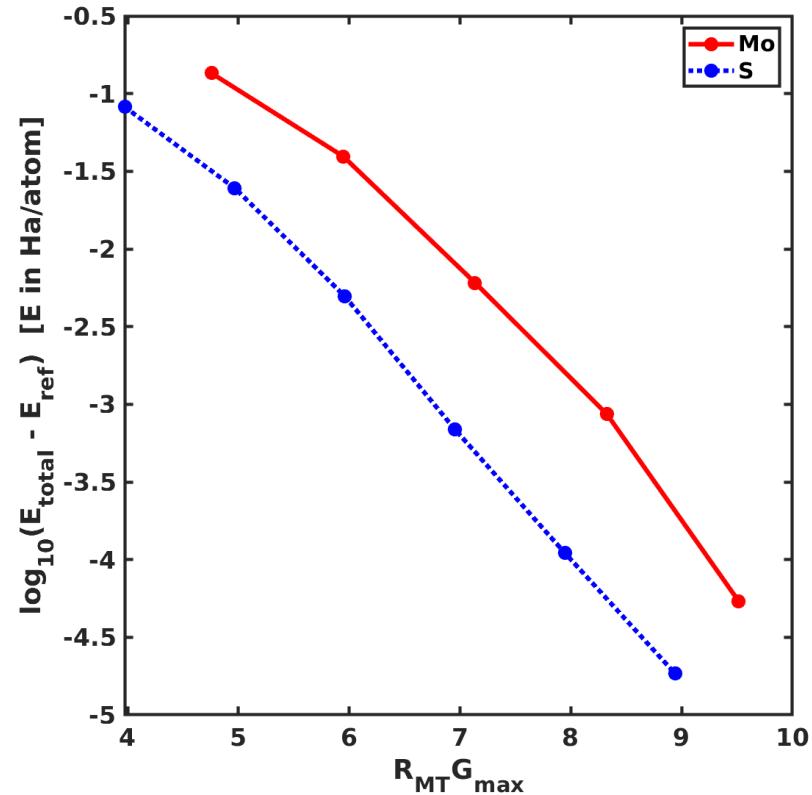
# APW+lo: influence of muffin-tin radii



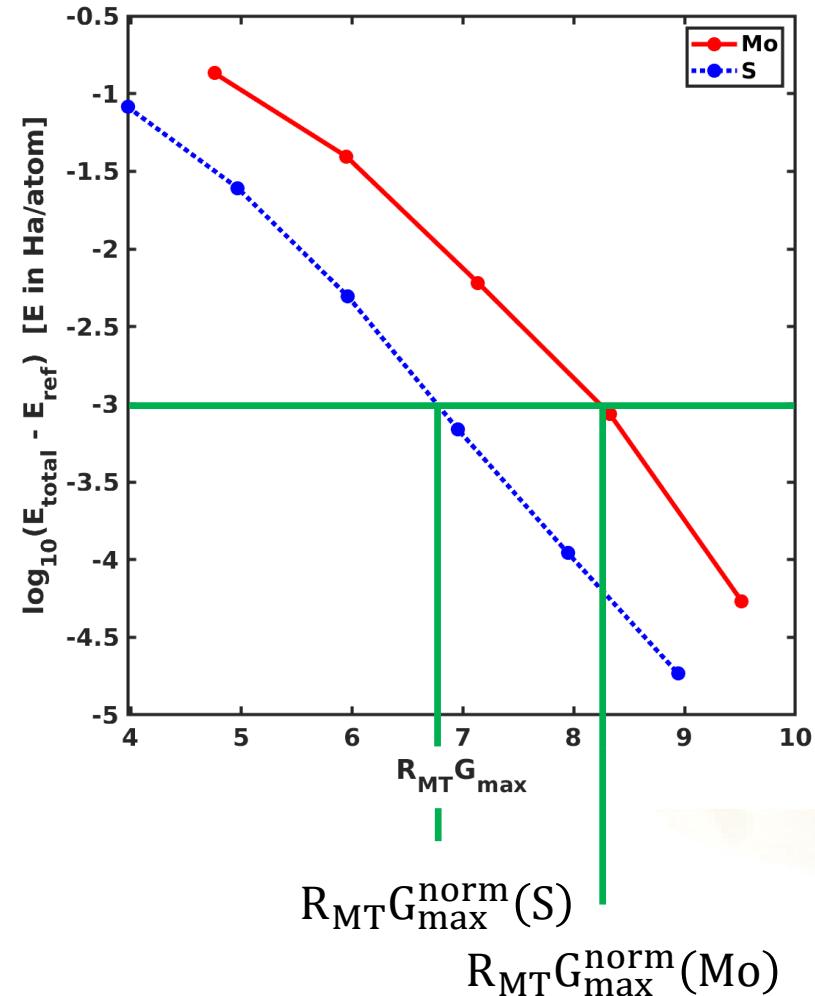
# Ratios of muffin-tin radii in compound crystals



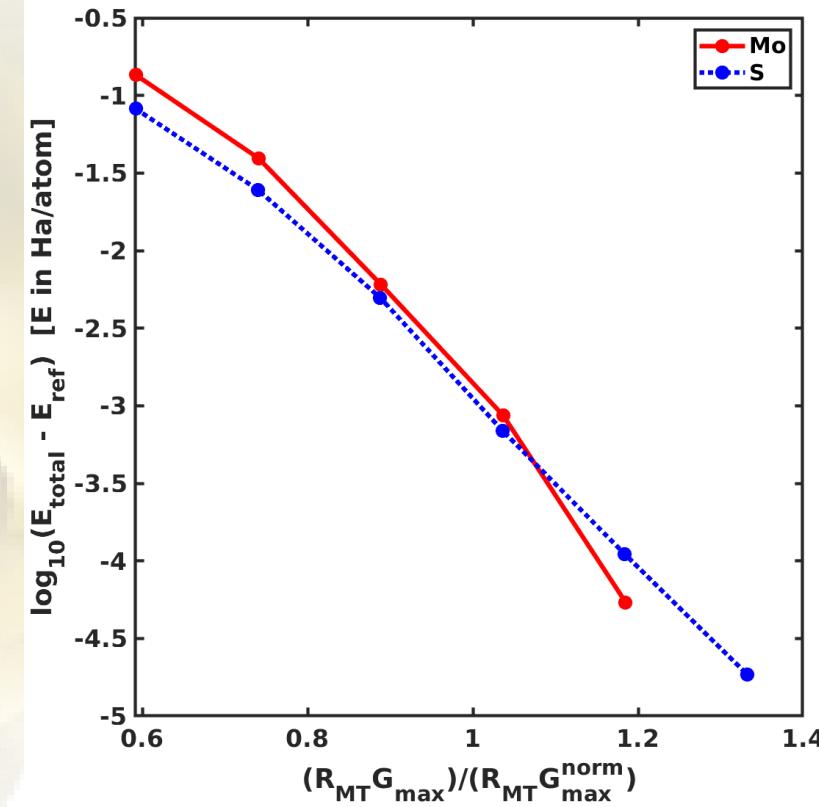
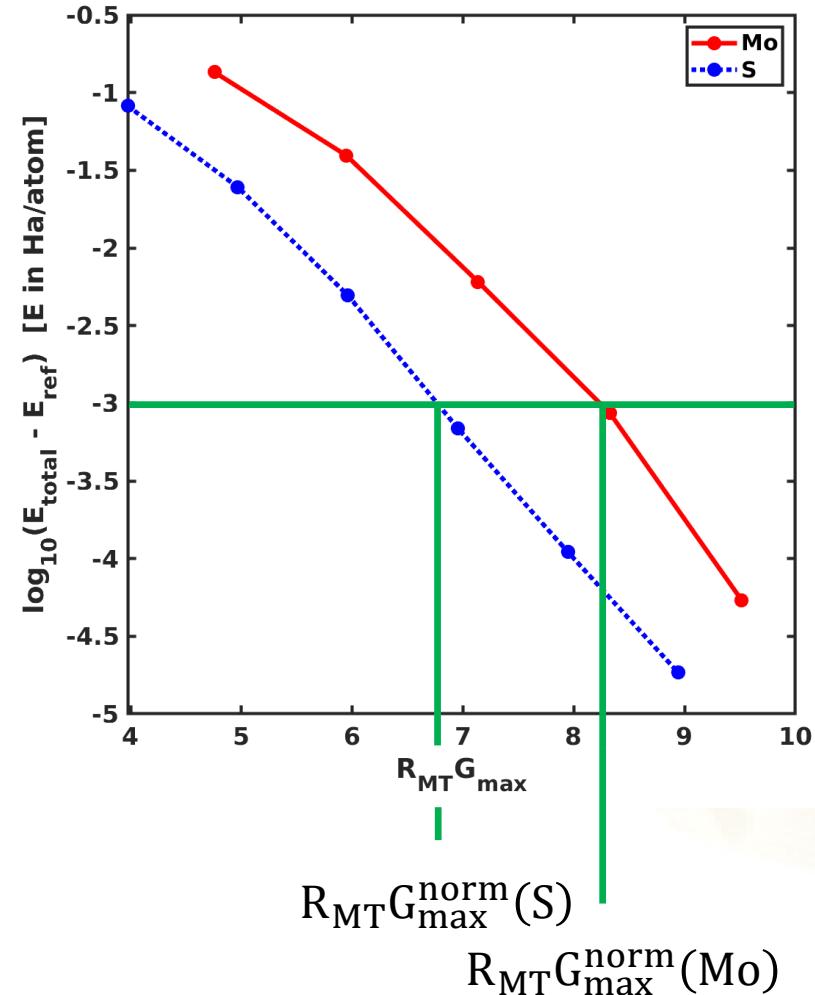
# Each element has “personal” $R_{MT}G_{max}$ behavior



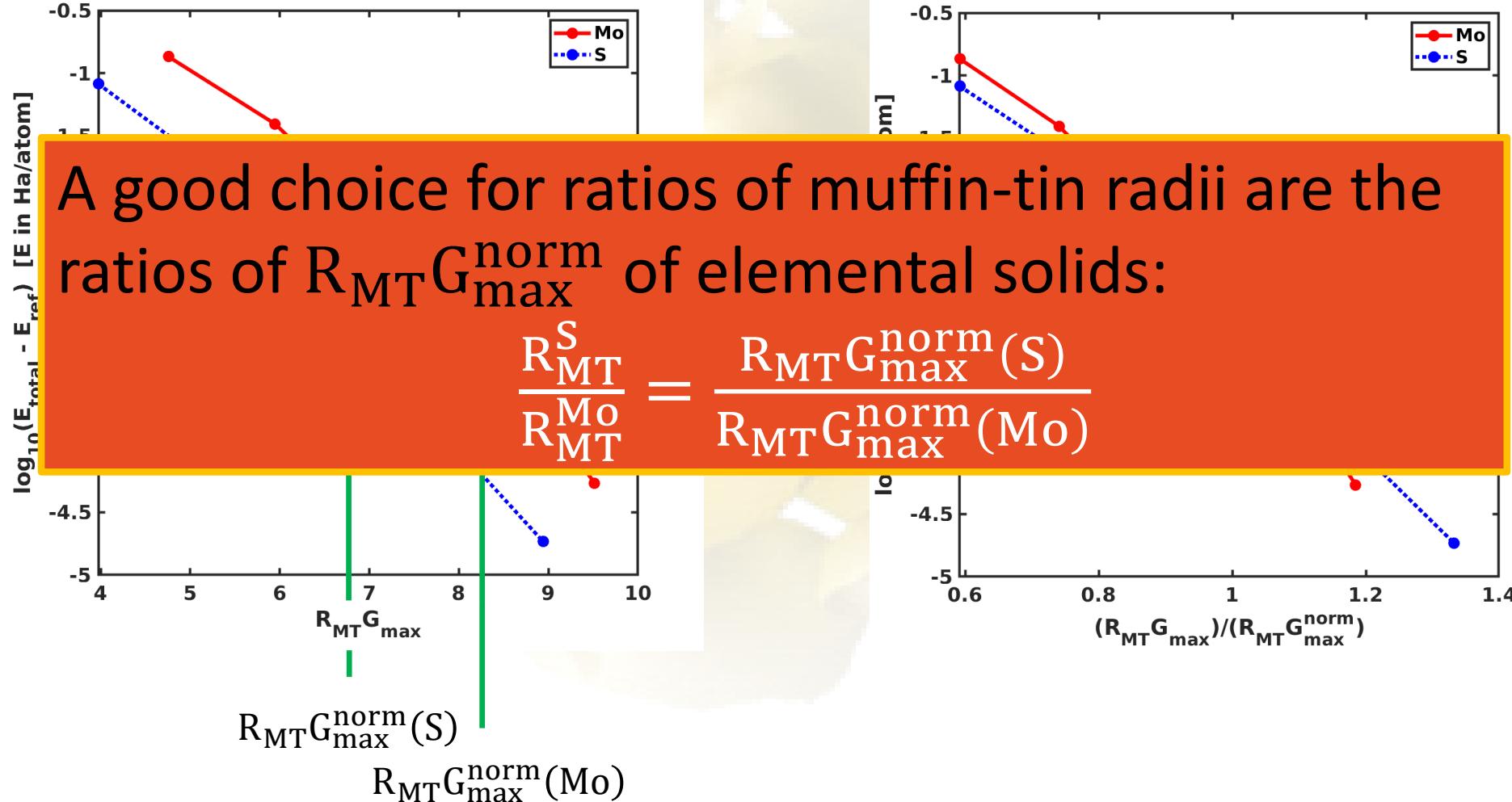
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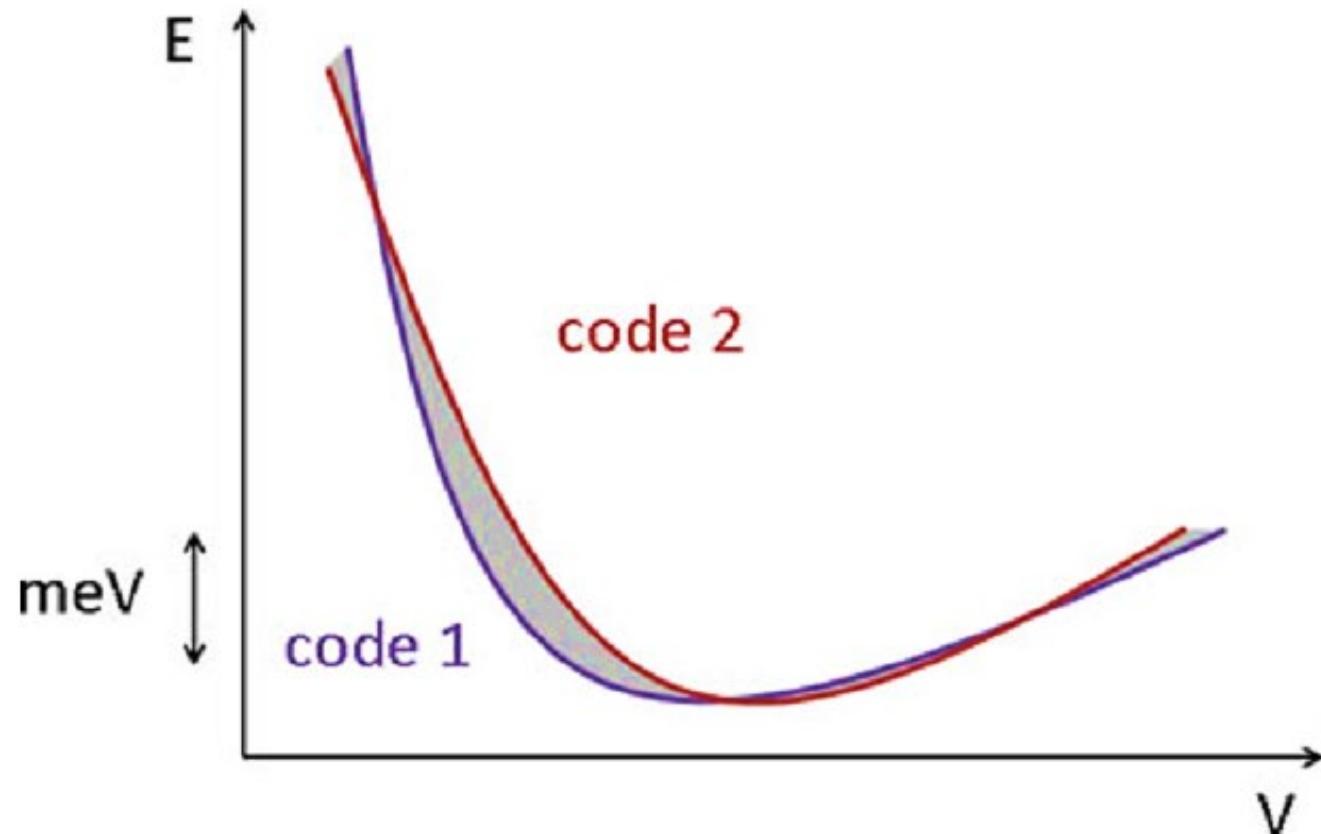
# Each element has “personal” $R_{MT}G_{max}$ behavior



# Benchmark Set: 71 Elemental Crystals

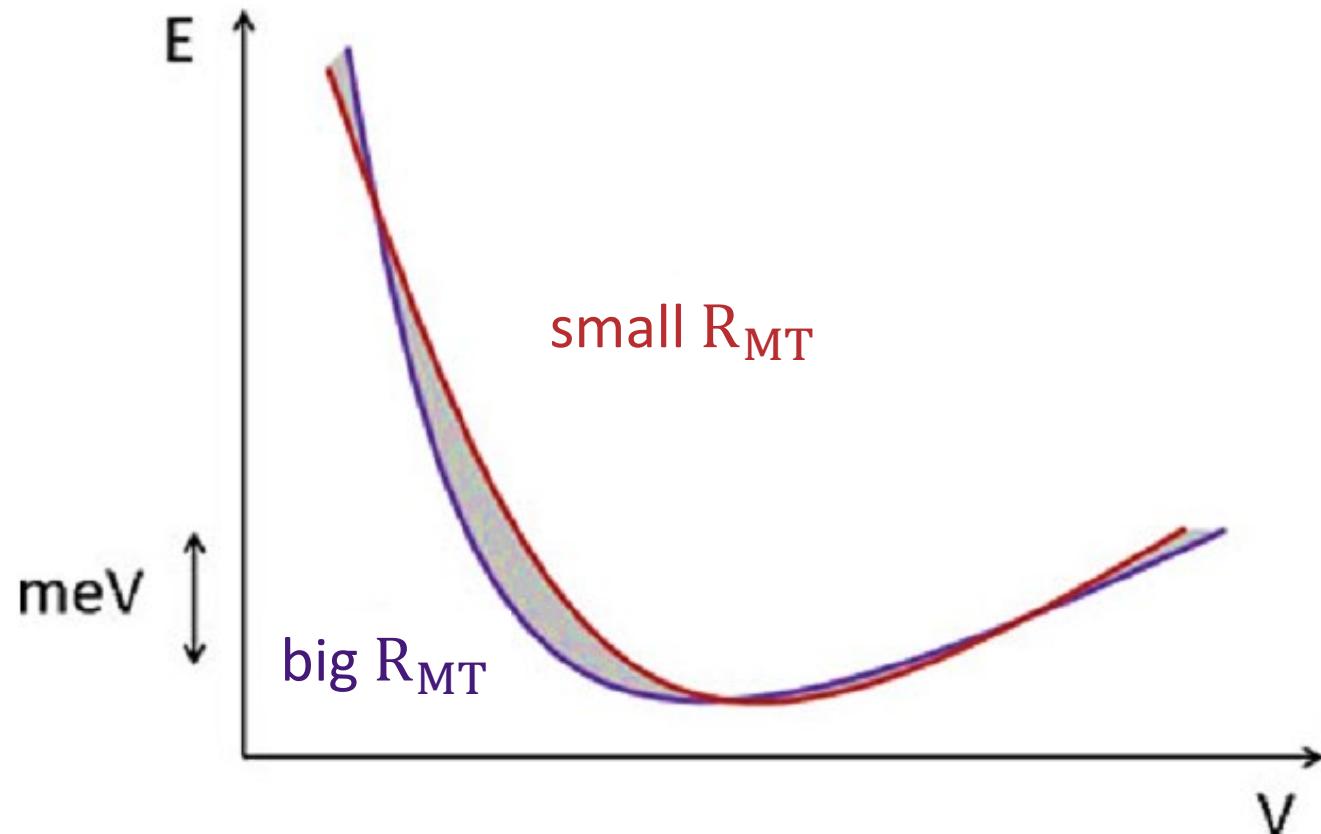
H	symbol space group Pearson (non-)magnetic														He		
194															194		
hP4															hP2		
nm															nm		
Li	Be																
166	194																
hR9	hP2																
nm	nm																
Na	Mg																
166	194																
hR9	hP2																
nm	nm																
K	Ca	Sc	Ti	V	Cr	Mn	Fe	Co	Ni	Cu	Zn	Ga	Ge	As	Se	Br	Kr
229	225	194	194	229	229	225	229	194	225	225	194	64	227	166	152	64	225
cl2	cF4	hP2	hP2	cl2	cl2	cF4	cl2	hP2	cF4	cF4	hP2	oS8	cF8	hR6	hP3	oS8	cF4
nm	nm	nm	nm	nm	afm	afm	fm	fm	fm	nm							
Rb	Sr	Y	Zr	Nb	Mo	Tc	Ru	Rh	Pd	Ag	Cd	In	Sn	Sb	Te	I	Xe
229	225	194	194	229	229	194	194	225	225	225	194	139	227	166	152	64	225
cl2	cF4	hP2	hP2	cl2	cl2	hP2	hP2	cF4	cF4	cF4	hP2	tl2	cF8	hR6	hP3	oS8	cF4
nm	nm	nm	nm	nm	nm	nm	nm	nm	nm	nm	nm	nm	nm	nm	nm	nm	nm
Cs	Ba	Lu	Hf	Ta	W	Re	Os	Ir	Pt	Au	Hg	Tl	Pb	Bi	Po	At	Rn
229	229	194	194	229	229	194	194	225	225	225	139	194	225	166	221		225
cl2	cl2	hP2	hP2	cl2	cl2	hP2	hP2	cF4	cF4	cF4	tl2	hP2	cF4	hR6	cP1		cF4
nm	nm	nm	nm	nm	nm	nm	nm	nm	nm	nm	nm	nm	nm	nm		nm	

# Quality factor



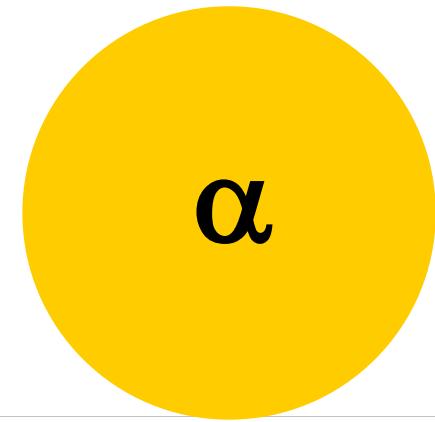
$$\Delta = \sqrt{\left\langle \frac{\int \Delta E^2(V) dV}{\Delta V} \right\rangle}$$

# Quality factor



$$\Delta = \sqrt{\left\langle \frac{\int \Delta E^2(V) dV}{\Delta V} \right\rangle}$$

# Test Basis Completeness



$\Delta$ -factors are shown in meV/atom

$$\Delta_{\text{mean}} = 0.008 \text{ meV/atom}$$
$$\Delta_{\text{max}} = 0.041 \text{ meV/atom}$$

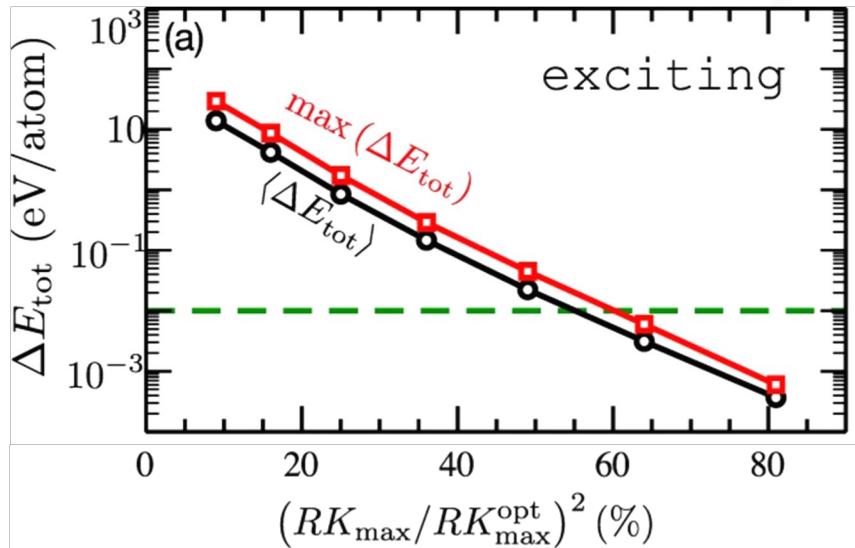
H		$\Delta$ -factors are shown in meV/atom														He	
0.000																0.000	
Li	Be																Ne
0.001	0.004																0.004
Na	Mg																Ar
0.001	0.000																0.002
K	Ca	Sc	Ti	V	Cr	Mn	Fe	Co	Ni	Cu	Zn	Ga	Ge	As	Se	Br	Kr
0.003	0.012	0.002	0.003	0.015	0.008	0.026	0.009	0.011	0.016	0.018	0.009	0.004	0.002	0.018	0.022	0.004	0.002
Rb	Sr	Y	Zr	Nb	Mo	Tc	Ru	Rh	Pd	Ag	Cd	In	Sn	Sb	Te	I	Xe
0.003	0.001	0.000	0.003	0.010	0.009	0.004	0.007	0.009	0.031	0.006	0.013	0.001	0.001	0.003	0.005	0.013	0.001
Cs	Ba	Lu	Hf	Ta	W	Re	Os	Ir	Pt	Au	Hg	Tl	Pb	Bi	Po	At	Rn
0.000	0.001	0.026	0.040	0.041	0.009	0.016	0.013	0.020	0.023	0.002	0.011	0.007	0.001	0.002	0.001		0.001

# Get $R_{MT}G_{max}^{norm}$ for each element

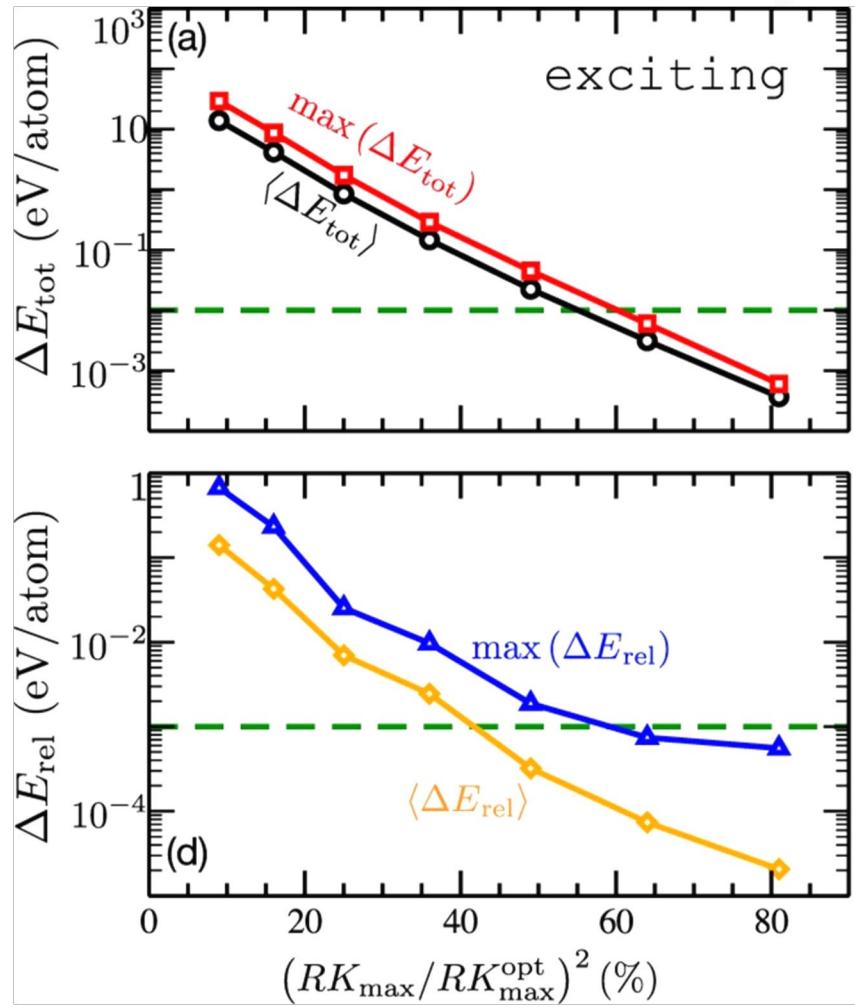
$$R_{MT}G_{max}^{norm} = R_{MT}G_{max} (\Delta E = 10^{-4} \text{eV/atom})$$

H 5.84																	He 8.23				
Li 8.45	Be 8.31															B 8.97	C 9.38	N 9.55	O 10.24	F 10.79	Ne 10.44
Na 10.64	Mg 10.58															Al 10.21	Si 10.61	P 10.36	S 9.93	Cl 10.22	Ar 10.47
K 10.88	Ca 10.77	Sc 11.58	Ti 11.80	V 11.92	Cr 12.26	Mn 12.42	Fe 12.57	Co 12.69	Ni 12.78	Cu 12.62	Zn 12.75	Ga 12.68	Ge 12.80	As 12.79	Se 12.90	Br 12.40	Kr 10.60				
Rb 11.35	Sr 10.86	Y 11.32	Zr 11.66	Nb 11.86	Mo 11.89	Tc 12.31	Ru 12.55	Rh 12.74	Pd 12.88	Ag 13.03	Cd 13.08	In 13.23	Sn 13.45	Sb 13.50	Te 13.26	I 13.43	Xe 11.33				
Cs 13.34	Ba 13.01	Lu 15.13	Hf 14.96	Ta 14.61	W 13.93	Re 13.65	Os 13.63	Ir 13.45	Pt 13.07	Au 13.23	Hg 13.26	Tl 13.37	Pb 13.56	Bi 13.57	Po 13.58	At 12.27	Rn				

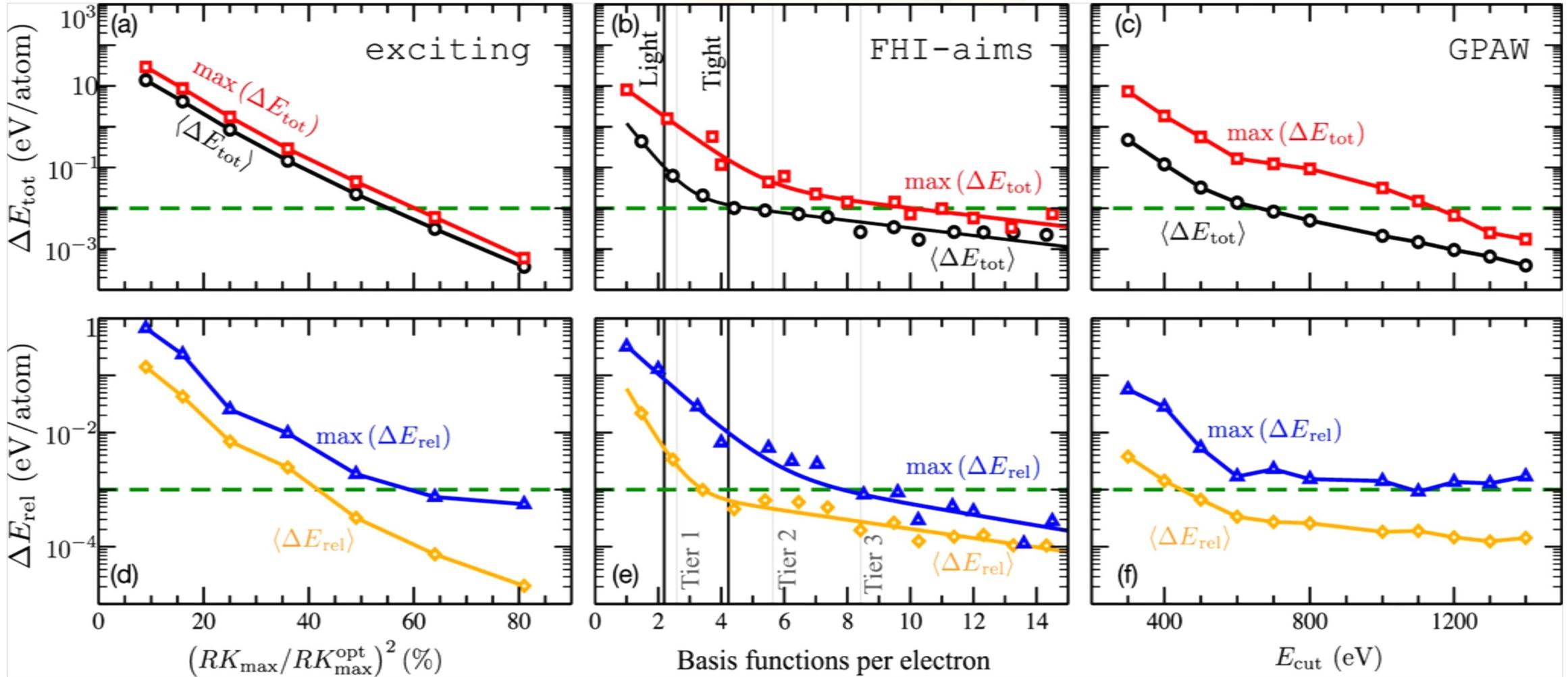
# Energy convergence



# Energy convergence



# Energy convergence



# Predict Numerical Errors of Any Material Using Errors of Elemental Solids

Predicted error for  
a general solid

$$\widehat{\Delta E} = \frac{1}{N} \sum_I N_I \Delta E_I$$

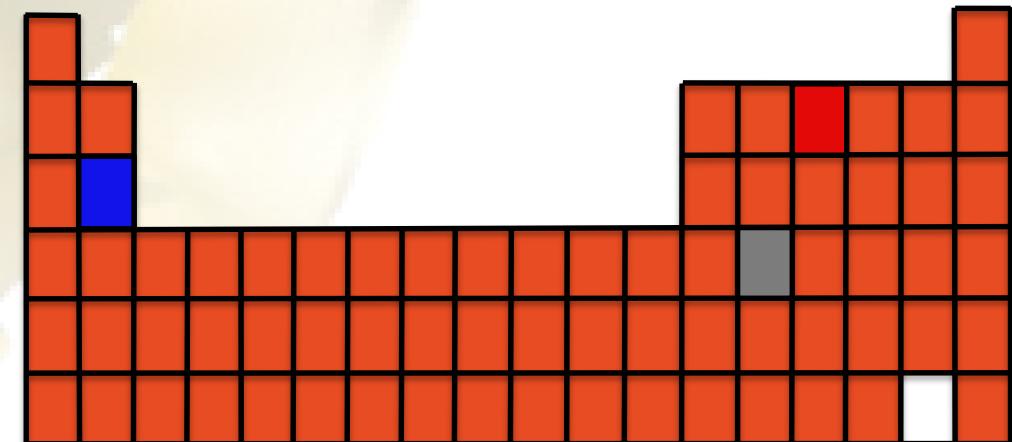
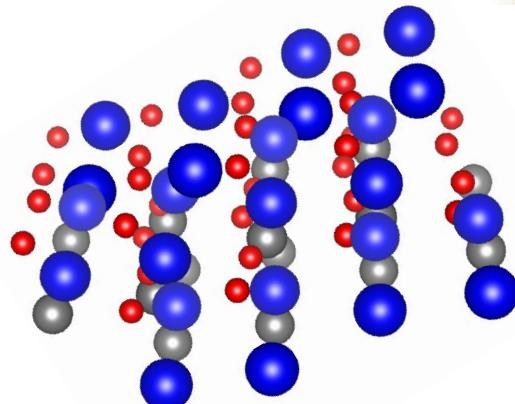
Observed error in  
elemental solids

# Predict Numerical Errors of Any Material Using Errors of Elemental Solids

Predicted error for  
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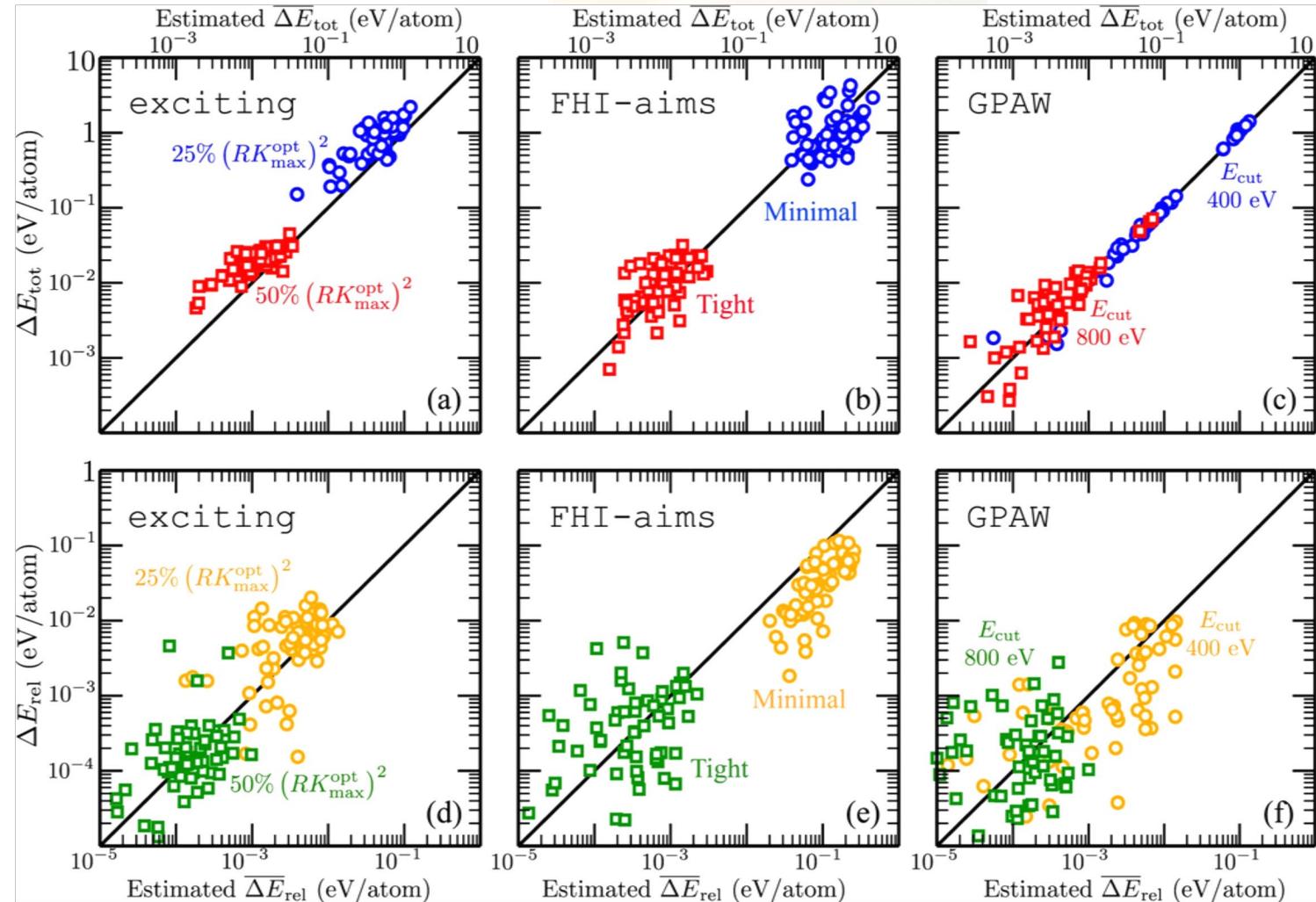
$$\hat{\Delta}E = \frac{1}{N} \sum_I N_I \Delta E_I$$

Observed error in  
elemental solids

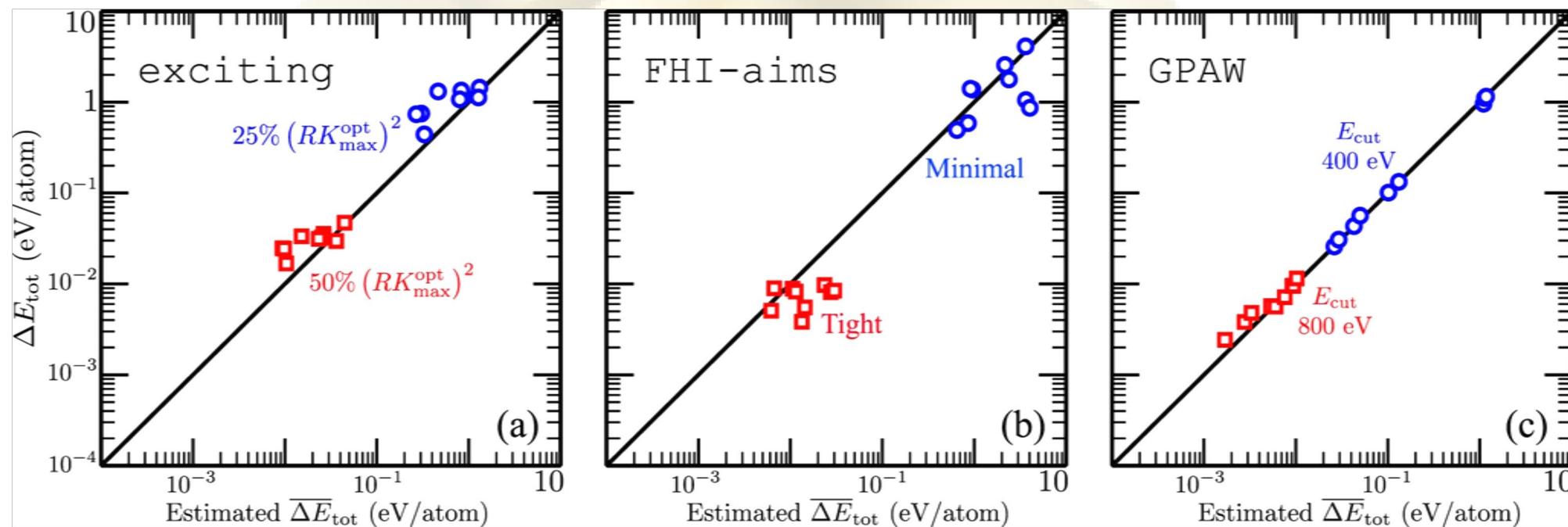


$$\hat{\Delta}E_{\text{GeMgN}_2} = \frac{1}{4} (\Delta E_{\text{Ge}} + \Delta E_{\text{Mg}} + 2\Delta E_{\text{N}})$$

# Numerical error prediction for 63 binary systems



# Numerical error prediction for ternary systems



# Conclusion

- Second order energy derivatives in los help to make results more independent of numerical parameters like linearization energies and muffin-tin radii
- An element's "personal"  $R_{MT}G_{max}$  behavior of its error in total energy is transferable to more complex compound crystals
- Tabulated  $R_{MT}G_{max}^{norm}$  of elemental solids can be used to make APW input parameters more material independent
- $\widehat{\Delta E} = \frac{1}{N} \sum_I N_I \Delta E_I$  allows us to estimate numerical errors for arbitrary systems